



Figure D-1.

The variables are

- m_b is the block mass,
- k is the spring stiffness,
- μ is mass density (mass/length) of the spring,
- L_s is the length of the spring,
- m_p is the pendulum mass,
- L_p is the pendulum length,
- x is the absolute displacement of the mass,
- θ is the pendulum angular displacement.

The total potential energy is

$$PE = \frac{1}{2} kx^2 + m_p g L_p (1 - \cos \theta) \quad (D-1)$$

The total kinetic energy is

$$KE = \frac{1}{2} m_b \dot{x}^2 + \frac{1}{6} \mu \dot{x}^2 L_s + \frac{1}{2} m_p (L_p \dot{\theta} + \dot{x})^2 \quad (D-2)$$

Apply the energy method.

$$\frac{d}{dt} \left\{ \frac{1}{2} m_b \dot{x}^2 + \frac{1}{6} \mu \dot{x}^2 L_s + \frac{1}{2} m_p (L_p \dot{\theta} + \dot{x})^2 + \frac{1}{2} kx^2 + m_p g L_p (1 - \cos \theta) \right\} = 0 \quad (D-3)$$

$$m_b \dot{x} \ddot{x} + \frac{1}{3} \mu \dot{x} \ddot{x} L_s + m_p (L_p \dot{\theta} + \dot{x})(L_p \ddot{\theta} + \ddot{x}) + kx \dot{x} + m_p g L_p (\sin \theta) \dot{\theta} = 0 \quad (D-4)$$

$$m_b \dot{x} \ddot{x} + \frac{1}{3} \mu \dot{x} \ddot{x} L_s + m_p L_p^2 \dot{\theta} \ddot{\theta} + m_p L_p \dot{\theta} \ddot{x} + m_p L_p \ddot{\theta} \dot{x} + m_p \dot{x} \ddot{x} + kx \dot{x} + m_p g L_p (\sin \theta) \dot{\theta} = 0 \quad (D-5)$$

For small angles,

$$\sin \theta \approx \theta \quad (D-6)$$

Thus,

$$m_b \dot{x} \ddot{x} + \frac{1}{3} \mu \dot{x} \ddot{x} L_s + m_p L_p^2 \dot{\theta} \ddot{\theta} + m_p L_p \dot{\theta} \ddot{x} + m_p L_p \ddot{\theta} \dot{x} + m_p \dot{x} \ddot{x} + kx \dot{x} + m_p g L_p \theta \dot{\theta} = 0 \quad (D-7)$$

$$\begin{aligned} & + \left\{ m_b \ddot{x} + \frac{1}{3} \mu \ddot{x} L_s + m_p L_p \ddot{\theta} + m_p \ddot{x} + kx \right\} \dot{x} \\ & + \left\{ m_p L_p^2 \ddot{\theta} + m_p L_p \ddot{x} + m_p g L_p \theta \right\} \dot{\theta} = 0 \end{aligned} \quad (D-8)$$

Equation (D-8) can be separated into two equations

$$\left\{ m_b \ddot{x} + \frac{1}{3} \mu \ddot{x} L_s + m_p L_p \ddot{\theta} + m_p \ddot{x} + kx \right\} \dot{x} = 0 \quad (\text{D-9})$$

And

$$\left\{ m_p L_p^2 \ddot{\theta} + m_p L_p \ddot{x} + m_p g L_p \theta \right\} \dot{\theta} = 0 \quad (\text{D-10})$$

Divide each equation by its respect velocity term.

$$\left\{ m_b \ddot{x} + \frac{1}{3} \mu \ddot{x} L_s + m_p L_p \ddot{\theta} + m_p \ddot{x} + kx \right\} = 0 \quad (\text{D-11a})$$

$$\left\{ \left[m_b + m_p + \frac{1}{3} \mu L_s \right] \ddot{x} + m_p L_p \ddot{\theta} + kx \right\} = 0 \quad (\text{D-11b})$$

And

$$\left\{ m_p L_p^2 \ddot{\theta} + m_p L_p \ddot{x} + m_p g L_p \theta \right\} = 0 \quad (\text{D-12a})$$

$$\left\{ m_p L_p \ddot{\theta} + m_p \ddot{x} + m_p g \theta \right\} = 0 \quad (\text{D-12b})$$

$$\left\{ L_p \ddot{\theta} + \ddot{x} + g \theta \right\} = 0 \quad (\text{D-12c})$$

Assemble the equations in matrix form.

$$\begin{bmatrix} \left[m_b + m_p + \frac{1}{3} \mu L_s \right] \\ 1 \end{bmatrix} \begin{matrix} m_p \\ 1 \end{matrix} \begin{bmatrix} \ddot{x} \\ \ddot{\theta} L_p \end{bmatrix} + \begin{bmatrix} k \\ 0 \end{bmatrix} \begin{bmatrix} x \\ \theta \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad (\text{D-13})$$

Alternate Form

Again, the energy method can be used to derive the equation of motion. The following form can be used if the natural frequency is the only parameter of interest.

$$KE_1 + PE_1 = KE_2 + PE_2 \quad (E-1)$$

The subscripts represent time.

Conclusion

The energy method is suitable for reasonably simple systems.

The energy method may be inappropriate for complex systems, however. The reason is that the distribution of the vibration amplitude is required before the kinetic energy equation can be derived. Prior knowledge of the “mode shapes” is thus required.

The Lagrange method is better suited for complex systems, as discussed before.
